## High Frequency PWM Step-Up Regulator

## élantec.

The EL7512 is a high frequency, high efficiency step-up DC:DC regulator operated at fixed frequency PWM mode. With an integrated 1 A MOSFET, it can deliver up to 600 mA output current at up to $90 \%$ efficiency. The adjustable switching frequency is up to 1.2 MHz , making it ideal for DSL applications.

When shut down, it draws $<3 \mu \mathrm{~A}$ of current. This feature, along with the minimum starting voltage of 2 V , makes it suitable for portable equipment powered by one lithium ion or 3 to 4 NiMH cells.

The EL7512 is available in a 10-pin MSOP package, with maximum height of 1.1 mm . With proper external components, the whole converter takes less than $0.25 \mathrm{in}^{2}$ PCB space.

This device is specified for operation over the full $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range.

## Pinout

EL7512
(10-PIN MSOP)
TOP VIEW


## Features

- $90 \%$ efficiency
- Up to 600 mA Iout
- $5 \mathrm{~V}<\mathrm{V}_{\text {OUT }}<18 \mathrm{~V}$
- $\mathrm{V}_{\mathrm{IN}}>2 \mathrm{~V}$
- Up to 1.2 MHz adjustable frequency
- < $3 \mu \mathrm{~A}$ shutdown current
- Adjustable soft-start
- Low battery detection
- Internal thermal protection
- 1.1 mm max height 10-pin MSOP package


## Applications

- 3 V to $5 \mathrm{~V}, 12 \mathrm{~V}$, and 18 V converters
- 5 V to 12 V and 16 V converters
- TFT-LCD
- DSL
- Portable equipment
- Desktop equipment


## Ordering Information

| PART NUMBER | PACKAGE |  <br> REEL | PKG. NO. |
| :--- | :---: | :---: | :---: |
| EL7512CY | 10-Pin MSOP | - | MDP0043 |
| EL7512CY-T7 | 10-Pin MSOP | $7 \prime \prime$ | MDP0043 |
| EL7512CY-T13 | 10-Pin MSOP | $13 "$ | MDP0043 |

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Absolute Maximum Ratings \(\left(\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right)\)
EN, LBI, . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . +18 C .
LX .................................................................. . . . 20 V
```



Storage Temperature
$-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Temperature . . . . . . . . . . . . . . . . . . . . . . . . $40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Operating Junction Temperature:. . . . . . . . . . . . . . . . . . . . . . . $135^{\circ} \mathrm{C}$

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore: $T_{J}=T_{C}=T_{A}$

Electrical Specifications $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{OUT}}=12 \mathrm{~V}, \mathrm{I}_{\mathrm{OUT}}=0 \mathrm{~mA}, \mathrm{R}_{\mathrm{T}}=100 \mathrm{k} \Omega, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise specified.

| PARAMETER | DESCRIPTION | CONDITION | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IQ1 | Quiescent Current - Shut-down | $\mathrm{VEN}=0$ |  |  | 3 | $\mu \mathrm{A}$ |
| IQ2 | Quiensent Current | $V E N=2 V$ |  | 2.5 | 4 | mA |
| VFB | Feedback Voltage |  | 1.31 | 1.35 | 1.39 | V |
| IB | Feedback Input Bias Current |  |  |  | 0.10 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {IN }}$ | Input Voltage Range |  | 2 |  |  | V |
| D MAX | Maximum Duty Cycle |  | 84 | 90 |  | \% |
| ILIM | Current Limit - Max Average Input Current |  | 1000 | 1250 | 1500 | mA |
| ISHDN | Shut-down Input Bias Current |  |  |  | 1 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\mathrm{LBI}}$ | LBI Threshold Voltage |  | 180 | 220 | 250 | mV |
| $\mathrm{V}_{\text {OL-LBO }}$ | LBO Output Low | $\mathrm{ILBO}=1 \mathrm{~mA}$ |  | 0.1 | 0.2 | V |
| ILEAK-LBO | LBO Output Leakage Current | $\mathrm{VLBI}=250 \mathrm{mV}, \mathrm{VLBO}=5 \mathrm{~V}$ |  | 0.02 | 1 | $\mu \mathrm{A}$ |
| R ${ }_{\text {DS-ON }}$ | Switch On Resistance | at 12 V output |  | 300 |  | $\mathrm{m} \Omega$ |
| ILEAK-SWITCH | Switch Leakage Current |  |  |  | 1 | $\mu \mathrm{A}$ |
| $\Delta \mathrm{V}_{\text {OUT }} / \Delta \mathrm{V}_{\text {IN }}$ | Line Regulation | $3 \mathrm{~V}<\mathrm{V}_{\text {IN }}<6 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=12 \mathrm{~V}$, no load |  |  | 0.15 | \%/V |
| $\Delta \mathrm{V}_{\text {OUT }} / \Delta \mathrm{I}_{\text {OUT }}$ | Load Regulation | IOUT < 250mA |  | 0.5 |  | \% |
| FOSC-MAX | Maximum Switching Frequency | $\mathrm{R}_{\mathrm{T}}=49.9 \mathrm{k} \Omega$ |  | 1200 |  | kHz |
| FOSC1 | Switching Frequency |  | 530 | 670 | 800 | kHz |
| VHI_EN | EN Input High Threshold |  | 1.6 |  |  | V |
| VLO_EN | EN Input Low Threshold |  |  |  | 0.5 | V |

## Pin Descriptions

| PIN NUMBER | PIN NAME |  |
| :---: | :---: | :--- |
| 1 | PGND | Power ground; connected to the source of internal N-channel power MOSFET |
| 2 | SGND | Signal ground; ground reference for all the control circuitry; needs to have only a single connection to PGND |
| 3 | RT | Timing resistor to adjust the oscillation frequency of the converter |
| 4 | EN | Chip enable; connects to logic HI (>1.6V) for chip to function |
| 5 | LBI | Low battery input; connects to a sensing voltage, or left open if function is not used |
| 6 | LBO | Low battery detection output; connected to the open drain of a MOSFET; able to sink 1mA current |
| 7 | SS | Soft-start; connects to a capacitor to control the start-up of the converter |
| 8 | FB | Voltage feedback input; needs to connect to resistor divider to decide $\mathrm{V}_{\mathrm{O}}$ |
| 9 | VDD | Control circuit positive supply |
| 10 | LX | Inductor drive pin; connected to the drain of internal N-channel power MOSFET |

## Block Diagram



## Typical Performance Curves






$F_{\text {S }}$ vs Temperature


## Typical Performance Curves (Continued)



$I_{D D}$ vs $F_{S}$
 Seady State Operation (inductor continuous conduction) $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=12 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=300 \mathrm{~mA}$


Steady State Operation (inductor discontinuous conduction) $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=12 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=25 \mathrm{~mA}$



## Applications Information

The EL7512 is a step-up regulator, operated at fixed frequency pulse-width-modulation (PWM) control. The input voltage is $2 \mathrm{~V}-12 \mathrm{~V}$ and output voltage is $5 \mathrm{~V}-18 \mathrm{~V}$. The switching frequency (up to 1.2 MHz ) is decided by the resistor connected to RT pin.

## Start-Up

After $\mathrm{V}_{\mathrm{DD}}$ reaches a threshold of about 2 V , the start-up oscillator generates fixed duty-ratio of 0.5-0.7 at a frequency of several hundred kilohertz. This will boost the output voltage.
When $V_{D D}$ reaches about 3.7 V , the PWM comparator takes over the control. The duty ratio will be decided by the multiple-input direct summing comparator, Max_Duty signal (about 90\% duty-ratio), and the Current Limit Comparator, whichever is the smallest.

The soft-start is provided by the current limit comparator. As the internal $12 \mu \mathrm{~A}$ current source charges the external CSS, the peak MOSFET current is limited by the voltage on the capacitor. This in turn controls the rising rate of the output voltage.

The regulator goes through the start-up sequence as well after the EN signal is pulled to HI.

## Steady-State Operation

When the output reaches the preset voltage, the regulator operates at steady state. Depending on the input/output conditions and component values, the inductor operates at either continuous-conduction mode or discontinuousconduction mode.
In the continuous-conduction mode, the inductor current is a triangular waveform and LX voltage a pulse waveform. In the discontinuous-conduction mode, the inductor current is completely dried out before the MOSFET is turned on again. The input voltage source, the inductor, and the MOSFET and output diode parasitic capacitors forms a resonant circuit. Oscillation will occur in this period. This oscillation is normal and will not affect the regulation.

At very low load, the MOSFET will skip pulses sometimes. This is normal.

## Current Limit

The MOSFET current limit is nominally 1.2A and guaranteed 1 A. This restricts the maximum output current IOMAX based on the following formula:

$$
\mathrm{I}_{\text {OMAX }}=\left(1-\frac{\Delta \mathrm{I}_{\mathrm{L}}}{2}\right) \times \frac{\mathrm{V}_{\mathrm{IN}}}{\mathrm{~V}_{\mathrm{O}}}
$$

where:
$\Delta L_{\mathrm{L}}$ is the inductor peak-to-peak current ripple and is decided by:

$$
\Delta \mathrm{I}_{\mathrm{L}}=\frac{\mathrm{V}_{\mathrm{IN}}}{\mathrm{~L}} \times \frac{\mathrm{D}}{\mathrm{~F}_{\mathrm{S}}}
$$

$D$ is the MOSFET turn-on ratio and is decided by:

$$
\mathrm{D}=\frac{\mathrm{V}_{\mathrm{O}}-\mathrm{V}_{\mathrm{IN}}}{\mathrm{~V}_{\mathrm{O}}}
$$

$F_{S}$ is the switching frequency.
The following table gives typical values:
MAX CONTINUOUS OUTPUT CURRENTS

| $\mathbf{V}_{\mathbf{I N}}(\mathbf{V})$ | $\mathbf{V}_{\mathbf{O}}(\mathbf{V})$ | $\mathbf{L}(\boldsymbol{\mu H})$ | $F_{\mathbf{S}}(\mathbf{k H z})$ | $\mathbf{I} \mathbf{O M A X}$ <br> $(\mathbf{m A})$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 5 | 10 | 1000 | 360 |
| 2 | 9 | 10 | 1000 | 190 |
| 2 | 12 | 10 | 1000 | 140 |
| 3.3 | 5 | 10 | 1000 | 600 |
| 3.3 | 9 | 10 | 1000 | 310 |
| 3.3 | 12 | 10 | 1000 | 230 |
| 5 | 9 | 10 | 1000 | 470 |
| 5 | 12 | 10 | 1000 | 340 |
| 5 | 15 | 10 | 1000 | 260 |
| 9 | 12 | 10 | 1000 | 630 |
| 9 | 15 | 10 | 1000 | 470 |
| 12 | 15 | 10 | 1000 | 670 |
| 12 | 18 | 11 | 1000 | 510 |

## Component Considerations

It is recommended that $\mathrm{C}_{\mathrm{IN}}$ is larger than $10 \mu \mathrm{~F}$.
Theoretically, the input capacitor has ripple current of $\Delta \mathrm{L}_{\mathrm{L}}$. Due to high-frequency noise in the circuit, the input current ripple may exceed the theoretical value. Larger capacitor will reduce the ripple further.

The inductor has peak and average current decided by:

$$
\begin{aligned}
& \mathrm{I}_{\mathrm{LAVG}}=\frac{\mathrm{I}_{\mathrm{O}}}{1-\mathrm{D}} \\
& \mathrm{I}_{\mathrm{LPK}}=\mathrm{I}_{\mathrm{LAVG}}+\frac{\Delta \mathrm{I}_{\mathrm{L}}}{2}
\end{aligned}
$$

The inductor should be chosen to be able to handle this current. Furthermore, due to the fixed internal compensation, it is recommended that maximum inductance of $10 \mu \mathrm{H}$ and $15 \mu \mathrm{H}$ to be used in the 5 V and 12 V or higher output voltage, respectively.
The output diode has average current of $I_{0}$, and peak current the same as the inductor's peak current. Schottky
diode is recommended and it should be able to handle those currents.

Output voltage ripple is the product of peak inductor current times the ESR of output capacitor. Low ESR capacitor is to be used to reduce the output ripple. The minimum output capacitance of $330 \mu \mathrm{~F}, 47 \mu \mathrm{~F}$, and $33 \mu \mathrm{~F}$ is recommended for $5 \mathrm{~V}, 12 \mathrm{~V}$, and 16 V for 600 kHz switching frequency, respectively. For 1 MHz switching frequency, $220 \mu \mathrm{~F}, 33 \mu \mathrm{~F}$, and $22 \mu \mathrm{~F}$ capacitor can be used for the output voltages. In addition to the voltage rating, the output capacitor should also be able to handle the rms current is given by:

$$
\mathrm{I}_{\text {CORMS }}=\sqrt{(1-\mathrm{D}) \times\left(\mathrm{D}+\frac{\Delta \mathrm{I}_{\mathrm{L}}{ }^{2}}{\mathrm{I}_{\mathrm{LAVG}}{ }^{2}} \times \frac{1}{12}\right)} \times \mathrm{I}_{\mathrm{LAVG}}
$$

## Output Voltage

An external resistor divider is required to divide the output voltage down to the nominal reference voltage. The current drawn by the resistor network should be limited to maintain the overall converter efficiency. The maximum value of the resistor network is limited by the feedback input bias current and the potential for noise being coupled into the feedback pin. A resistor network less than $300 \mathrm{k} \Omega$ is recommended. The boost converter output voltage is determined by the relationship:

$$
\mathrm{V}_{\mathrm{OUT}}=\mathrm{V}_{\mathrm{FB}} \times\left(1+\frac{\mathrm{R}_{2}}{\mathrm{R}_{1}}\right)
$$

where $\mathrm{V}_{\mathrm{FB}}$ slightly changes with $\mathrm{V}_{\mathrm{DD}}$. The curve is shown in this data sheet.

## RC Filter

The maximum voltage rating for the $\mathrm{V}_{\mathrm{DD}} \mathrm{pin}$ is 12 V and is recommended to be about 10 V for maximum efficiency to drive the internal MOSFET. The series resistor R4 in the RC filter connected to $\mathrm{V}_{\mathrm{DD}}$ can be utilized to reduce the voltage. If $V_{O}$ is larger than 10 V , then:

$$
\mathrm{R}_{4}=\frac{\mathrm{V}_{\mathrm{O}}-10}{\mathrm{I}_{\mathrm{DD}}}
$$

where $I_{D D}$ is shown in $I_{D D}$ vs $F_{S}$ curve. Otherwise, R4 can be $10 \Omega$ to $51 \Omega$ with $\mathrm{C} 4=0.1 \mu \mathrm{~F}$.

## Thermal Performance

The EL7512 uses a fused-lead package, which has a reduced $\theta_{\mathrm{JA}}$ of $100^{\circ} \mathrm{C} / \mathrm{W}$ on a four-layer board and $115^{\circ} \mathrm{C} / \mathrm{W}$ on a two-layer board. Maximizing copper around the ground pins will improve the thermal performance.
This chip also has internal thermal shut-down set at around $135^{\circ} \mathrm{C}$ to protect the component.

## Layout Considerations

The layout is very important for the converter to function properly. Power Ground ( $\stackrel{\downarrow}{\mathrm{b}}$ ) and Signal Ground ( $\stackrel{\perp}{=}$ ) should be separated to ensure that the high pulse current in the Power Ground never interferes with the sensitive signals connected to Signal Ground. They should only be connected at one point.

The trace connected to pin $8(\mathrm{FB})$ is the most sensitive trace. It needs to be as short as possible and in a "quiet" place, preferably between PGND or SGND traces.

In addition, the bypass capacitor connected to the $\mathrm{V}_{\mathrm{DD}}$ pin needs to be as close to the pin as possible.

The heat of the chip is mainly dissipated through the SGND pin. Maximizing the copper area around it is preferable. In addition, a solid ground plane is always helpful for the EMI performance.

The demo board is a good example of layout based on these principles. Please refer to the EL7512 Application Brief for the layout.

## Package Outline Drawing



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